[Contribution from the Department of Chemical Engineering of the Massachusetts Institute of Technology]

Vapor-Adsorbate¹ Equilibrium. I. Propane-Propylene on Activated Carbon and on Silica Gel

BY W. K. LEWIS, E. R. GILLILAND, B. CHERTOW AND W. H. HOFFMAN

The potentiality of separating gases on an industrial scale by adsorptive procedures has led to a study of the equilibria involved when gaseous mixtures of hydrocarbons are in contact with solids of large specific surface area. In these investigations the adsorption isotherms of the individual components, and, in the case of the mixtures, the composition of the vapor and adsorbate in equilibrium with each other, have been determined. The condition of equilibrium has been ascertained, in dealing with mixtures, by approaching the equilibrium from both sides, *i. e.*, a given adsorbate composition would be attained by placing either gas (of a binary system) in contact with the adsorbent and equilibrating by bringing the second gas into contact with the solid. Finally, the reversibility of the phenomena has been investigated by desorption isotherms in the case of the individual components and by desorption and analysis of the adsorbed mixtures.

This report presents the results obtained when gaseous mixtures of propane and propylene were permitted to equilibrate with an activated carbon or a silica gel at $25.0 \pm 0.1^{\circ}$ and barometric pressure. The propane-propylene system is of interest because the physical properties of these gases are very similar and separation by a standard distillation technique is difficult.

Materials.—Commercial cylinders of C. P. grade gases were employed. When 22% sulfuric acid containing mercuric sulfate was used as an analytical reagent for determining olefins,² the propylene was found to be 99.15% olefin and the propane was found to be 0.05% olefin. Refrigeration grade silica gel, 14/20 mesh, with a BET³ surface area of 751 sq. m. per g. (as determined by the usual low temperature adsorption of nitrogen) was supplied by the Davison Chemical Company of Baltimore. An activated carbon called Black Pearls I with a surface area, similarly determined, of 705 sq. m. per g. was supplied by the Godfrey L. Cabot Co. of Boston. Chemically pure, redistilled mercury was used as the displacing fluid in the apparatus, and the tubing to connect the mercury leveling bulbs to the Pyrex glass apparatus was sulfur-free gum rubber or neoprene.

Apparatus.—The apparatus (Fig. 1) finally evolved consists of a gas measuring buret calibrated in 0.1 ml.

equipped with a compensator manometer to correct for temperature and barometer changes during an experiment. The first gas brought into the buret can then be stored in the premix chamber while the second gas is being measured. The gases are mixed by manipulation of the externally mounted bar magnets which causes spinning and raising (or lowering) of the soft iron washer within the glass chamber. The reservoir downstream of the adsorption U-tube permits the gases to be pumped back and forth over the adsorbent from the premix chamber to the reservoir, constancy of pressure being attained by maintaining the mercury level in the reservoir at the level of the mercury in the manometer leg.

By proper manipulation of the stopcock on the premix chamber, this unit may be employed as a desorption pump. If communication with the adsorption zone is brought about, when the level of mercury in this chamber is high, subsequent lowering of the mercury level causes the gas to be pumped into the chamber. After the stopcock is closed, the entrapped gases can be compressed to one atmosphere, pumped into the buret and measured. Repeated desorptions can create a very low pressure in the adsorption zone, since the volume of this zone is generally under 10 ml. while the premix chamber volume is 350 ml.

Glass to glass seals are used throughout except for the connection to the leveling bulbs. Precision bore, high vacuum stopcocks with mercury seals were employed with very small quantities of Apiezon M as lubricant. All capillaries shown in the diagram are 2-mm. bore, elsewhere the bore is 6 or 8 mm. Auxiliary apparatus consisted of a conventional Orsat type gas analysis assembly, a Cenco Hyvac pump for routine evacuations, a thermostat bath with a circulatory pump, $a 30^{\circ}$ thermometer calibrated in 0.1°, a Tesla coil for checking the evacuated apparatus, specially made clamps for regulating the flow of mercury through the rubber tubing, etc.

Procedure .- Experience in this Laboratory has taught that when a fresh sample of adsorbent is to be employed in adsorption studies, if a high degree reproducibility and reversibility of the phenomena are to be realized, the ad-sorbent surface must be "flushed" at least twice with one of the components of the gas mixture under investigation. Earlier workers in the field⁴ have also made this finding; it is reported because it must not be overlooked. Flushing the surface involves a preliminary evacuation of the adsorb-ent at an elevated temperature (refluxing glycol at 192° for activated carbon, and glycol-water at 160° for silica gel have been found satisfactory) followed by cooling, saturating the surface with one of the gases to be used and re-evacuation at the proper temperature. This technique is strikingly analogous to rinsing an analytical buret with the standard reagent to be measured by that buret. After at least two such flushings of the fresh adsorbent sample, routine desorption in preparation for an experiment merely consists in evacuating at the proper temperature for a period of one hour.

The gas volume (called hereafter the dead space) surrounding the adsorbent is determined by admitting a known volume of helium to the evacuated adsorption zone (maintained at $25.0 \pm 0.1^{\circ}$) and recording the pressure.

After the system is flushed and the dead space is determined, the system is again evacuated. Adsorption isotherms of the individual gases are determined by admitting successive small known quantities of gas to the adsorption zone and recording the pressure after a ten to fifteen minute wait for equilibrium. After the pressure in the

(4) H. S. Harned, ibid., 42, 372 (1920).

⁽¹⁾ The word adsorbate is used in this article to indicate material held by the solid.

⁽²⁾ Francis and Lukasiewics, Ind. Eng. Chem., Anal. Ed., 17, 703 (1945).

⁽³⁾ Brunauer, Emmett and Teller, THIS JOURNAL, **60**, 309-319 (1938).



Fig. 1.-Apparatus for determining vapor-adsorbate equilibrium.

adsorption zone has been built up to the maximum desired pressure, successive small quantities are desorbed with the desorption pump and are measured in the gas buret, pressures in the adsorption zone again being recorded. The reversibility of the phenomenon is thus checked. At $25.0 \pm 0.1^\circ$, the desorption isotherm can be readily studied down to a pressure of 2 mm. of mercury abs. To attain further desorption it is expeditious to raise the temperature in the adsorption zone.

When mixture runs are to be carried out with either a new adsorbent or new gas system, it is advisable to devote the first two experiments to finding out whether the same equilibrium values for the adsorbate and gas phase compositions are attainable independent of which gas has been on the surface first. Hence, the first experiment involves adding a known volume of the first gaseous component to the evacuated adsorption U-tube and permitting about forty minutes residence therein before adding a known volume of the second gas to the system. (Note, no premixing is employed in these initial experiments.) Passes back and forth through the U-tube for forty to sixty minutes (two or three minutes per pass) are generally The unadsorbed gas is then measured in the sufficient. buret and is analyzed. After re-evacuation of the adsorp tion zone at the proper temperature level, the same pro-cedure is repeated, this time, however, the order in which the gases are fed to the system is reversed.

If the two equilibrium values thus obtained lie close to one another this procedure of adding first one gas then the other may be followed throughout, or the premix chamber may be used as described above before any gas is admitted to the evacuated adsorption zone.

Reversibility of the adsorption of mixtures is readily determined by using the premix chamber as a desorption pump as described above. In general, it is best to pump off as much gas as possible before raising the temperature in the bath surrounding the adsorption zone. The desorbed gases can be measured in the buret and analyzed.

Results.—The data for the adsorption isotherms of propane and of propylene on silica gel and on activated carbon at $25.0 \pm 0.1^{\circ}$ are in Tables I and II, respectively, and are presented graphically in Fig. 2. The results for mixtures of these gases on the adsorbents mentioned are to be found in Table III and in Fig. 3, equilibrium distribution and total adsorption being shown.

TABLE I

Adsorption Isotherms of Propane on Activated Carbon (GLC) and Silica Gel at $25.0 \pm 0.1^{\circ}$

n =millimoles adsorbed per g. adsorbent; P =pressure,

| | | mm. | abs. | | |
|---------------------|-------|-------------|--------|--------------------------|--------|
| Carbon ^a | | Silica gelb | | Silica gel Desorption | |
| P, mm. | nc | P, mm. | nc | P, mm. | n° |
| 15.7^{d} | 0.791 | 11.1 | 0.0564 | 703.0 | 1.501 |
| 44.0 | 1.141 | 25.0 | .1252 | 611.1 | 1.350 |
| 54.2 | 1.223 | 43.5 | .1980 | 505.9 | 1.199 |
| 84.0 | 1.416 | 71.4 | . 2986 | 419.0 | 1.061 |
| 107.0^{d} | 1.532 | 100.0 | .3850 | 118.3 | 0.456 |
| 139.0 | 1.646 | 158.9 | .5441 | 57.2 | . 2690 |
| 177.0 | 1.769 | 227.5 | .7020 | 35.1 | .1912 |
| 215.5 | 1.872 | 304.2 | .843 | 12.0 | .0931 |
| 278.0 | 2.006 | 387.0 | 1.010 | 4.5 | . 0436 |
| 331.5 | 2.105 | 468.0 | 1.138 | | |
| 429.5^{d} | 2.254 | 569.0 | 1.288 | | |
| 536.0 | 2.373 | 677.8 | 1.434 | | |
| 585.7 | 2.454 | 775.0 | 1.562 | | |
| 640.7 ^d | 2.479 | | | | |
| 680.2 | 2.510 | | | | |

^a Vol. of dead space = 7.70 ml. ^b Vol. of dead space = 6.76 ml. ^e Based on adsorbent weight as received. Three to five per cent. of the as received adsorbent is easily removable volatile matter. The "as received" basis is used throughout this series. ^d Obtained on duplicate run of adsorption isotherms.



Fig. 2.--Adsorption isotherms of propane and propylene on activated carbon and on silica gel at $25.0 \pm 0.1^{\circ}$: $\nabla \triangle O \Box$, adsorption; $\nabla \triangle$, duplicate isotherm; $\bigcirc \blacksquare$, desorption.

Randomly chosen results on the data obtained when desorptions were carried out with the desorption pump are found in Table IV.

TABLE II

Adsorption Isotherms of Propylene on Activated Carbon (GLC) and Silica Gel at $25.0 \pm 0.1^{\circ}$ n = millimoles adsorbed per g. adsorbent. P = pressure.

| | | mm. | abs. | | pressure, | |
|---------------------|-------|------------|----------------|--------|------------|--|
| Carbon ^a | | _ | Silica gelb. c | | | |
| P, mm. | n | P, mm. | n | P, mm. | n | |
| Adsorption | | Adsorption | | Desc | Desorption | |
| 16.5 | 0.567 | 34.2 | 0.3738 | 650 | 2.073 | |
| 36.0ª | 1.107 | 71.4 | 0.7227 | 459 | 1.814 | |
| 47.7 | 1.171 | 91.6 | 0.7472 | 457.9 | 1.808 | |
| 71.0^{d} | 1.419 | 194.3 | 1.129 | 355.6 | 1.633 | |
| 118.5 | 1.648 | 198.3 | 1.168 | 281.8 | 1.473 | |
| 131.0 | 1.703 | 271.5 | 1.401 | 155.4 | 1.125 | |
| 154.0 | 1.786 | 253.2 | 1.562 | 74.2 | 0.7596 | |
| 192.0 | 1.913 | 550.7 | 1.918 | 4.4 | 0.1090 | |
| 231.0^{d} | 2.041 | 555.2 | 1.928 | | | |
| 294.0 | 2.168 | 760.6 | 2.184 | | | |
| | | | | | | |

| 398.5 | 2.366 | 768.2 | 2.197 |
|-------------|-------|-------|-------|
| 464.5^{d} | 2.456 | | |
| 537.5 | 2.552 | | |
| 649.5 | 2.677 | | |

^a See Table I. ^b See Table I. ^c Obtained with propylene containing 3.08% inert since the original propylene (0.85% inert) was consumed. ⁴ Duplicate isotherm.

All the results are based on using $PV = \mu RT$ as the equation of state of each gas. Values of μ were calculated from the ethylene charts of York.⁵

Precision of Results .-- The precision of the volumetric measurements should be high since the volumes measured usually exceeded 20 ml. and the burets employed are calibrated with 0.1 ml. marks. Hence, the precision desired governs the weight of the adsorbent sample, provided also the dead space is kept small compared to the total adsorption.



Fig. 3.-Isothermal, isobaric adsorption of propanepropylene mixtures on silica gel and on activated carbon; atmospheric pressure and 25°; total adsorption and vaporadsorbate equilibrium: \triangle O premixed gases, 20 passes; ∇ propane on surface first; \Box propylene on surface first: ▲ non-equilibrium, 2 passes on silica gel.

(5) R. York and E. F. White, Trans. Am. Inst. Chem. Eng., 40, 227 (1944).

TABLE III

Vapor-Adsorbate Equilibrium Data for Mixtures of Propane and Propylene over (1) Activated Carbon (GLC), (2) Silica Gel, at $25.0 \pm 0.1^{\circ}$ and Atmospheric Pressure (752-773 mm. abs.)

X = mole fraction of propane in adsorbate; Y = mole fraction of propane in gas phase; N = millimoles of mixture adsorbed per gram of adsorbent

| | Activated o | ausc | nbeu per gia | in or ausor ben | | e! | |
|------------------------------|-------------|-------|----------------|---------------------|--------|-------|-------|
| Y | X | N | π | Y | X | N | π |
| 0. 1104^{a,b} | 0.0993 | 2.819 | 755.6 | 0.2445° | 0.1078 | 2.197 | 769.2 |
| . 1881 ^{ª,b} | .1613 | 2.831 | 759.0 | . 299 | .2576 | 2.013 | 760.9 |
| . 2816 ^{a, b} | . 2596 | 2.823 | 760.0 | . 4040 ^b | . 2956 | 2.052 | 767.8 |
| .3799 ^{a,b} | .3675 | 2.907 | 757.0 | . 530 | .2816 | 2.041 | 761.0 |
| .3959ª | .3728 | 2.794 | 762.0 | . 5333* | .3655 | 1.963 | 753.6 |
| . 4328°, b | .4147 | 2.772 | 755.7 | . 5356ª | . 3120 | 1.967 | 766.3 |
| .4351°, ^b | . 4077 | 2.838 | 766.0 | .6140° | .3591 | 1.974 | 754.0 |
| $.4910^{a,b}$ | .4575 | 2.927 | 769.0 | .6220ª | . 5550 | 1.851 | 753.6 |
| . 5188ª | .4819 | 2.831 | 771.0 | .6252ª | .7007 | 1.701 | 754.0 |
| . 522ª | .5036 | 2.763 | 755.0 | .7480' | .723 | 1.686 | 760.0 |
| . 5460° | .6675 | 2.56 | 756.3 | .671 | .096 | 2.180 | |
| .5983*,* | .5865 | 2.793 | 759.0 | $.8964^{a}$ | . 253 | 1.993 | 760.0 |
| .6010 ^{a,b} | . 5925 | 2.777 | 756.5 | .921 | .401 | 1.426 | 760.0 |
| .6107ª | . 4112 | 2.605 | 756.9 | | | | |
| .6736 ^{a,b} | .6688 | 2.820 | 767.0 | | | | |
| .7577* | .7477 | 2.770 | 771.0 | | | | |
| .7695°, ^b | .7391 | 2.725 | 753.1 | | | | |
| .8410 ^{5,0} | .8315 | 2.768 | 76 3 .0 | | | | |
| .9158°, ^b | .8992 | 2.745 | 761.3 | | | | |
| .9528ª,b | .9517 | 2.670 | 772.4 | | | | |

^a Premixed gas, 20 passes. ^b Fresh sample of adsorbent used. ^c Propane on surface 1st for forty min., propylene added, 20 passes. ^d Propylene on surface 1st for forty min., propane added, 20 passes. ^c Premixed gas, 10 passes. ^f Premixed gas, 2 passes, non-equilibrium.

TABLE IV

DESORPTION RECOVERY OF PROPANE-PROPYLENE MIX-TURES

| | - | | |
|------|--------|-----|----------------|
| hete | Carbon | (CI | (\mathbf{n}) |

A

| Activated Carbon (GLC) | |
|--|--------|
| M1. of C_3H_8 fed to apparatus, S. T. P. | 24.74 |
| M1. of $C_{2}H_{6}$ fed to apparatus, S. T. P. | 115.85 |
| Total ml. fed to apparatus | 140.59 |
| Ml. of mix. retd. to buret, S. T. P. | 68.80 |
| M1. of evac. gas (adsorbate + dead space gas) | 72.00 |
| Total ml. recovered from apparatus | 140.80 |
| Silica Gel | |
| M1. of C_3H_8 fed to apparatus, S. T. P | 18.62 |
| M1. of C_3H_6 fed to apparatus, S. T. P. | 89.22 |
| Total ml. fed to apparatus | 107.84 |
| M1. of mix retd. to buret, S. T. P. | 44.01 |
| M1. of evac. gas | 63.37 |
| Total ml. recovered from apparatus | 107.38 |

Discussion.—The individual isotherms of propane and propylene, respectively, on the activated carbon appear to follow the empirical Freundlich equation somewhat better than the theoretical Langmuir⁶ equation. While the pressure range involved herein is mainly outside that suggested by Brunauer, *et al.*,⁸ the few points in this range do follow their relationship. Because none of these isotherm equations fit the data satisfactorily over the pressure range studied herein, none of the constants of the equations is reported, though over portions of the isotherms there is reasonable agreement with either the Freundlich or Langmuir equation.

(6) I. Langmuir, THIS JOURNAL, 38, 2221-2295 (1916).

The Langmuir adsorption equation for a binary mixture at equilibrium is given as

$$n_{p} = \frac{a_{p}b_{p}p_{p}}{1 + b_{0}p_{0} + b_{p}p_{p}} \text{ for the paraffin and}$$

$$n_{0} = \frac{a_{0}b_{0}p_{0}}{1 + b_{p}p_{p} + b_{0}p_{0}} \text{ for the olefin}$$

where n = millimoles of gas adsorbed per gram of adsorbent at a partial pressure in the mixture of p; a and b are constants and the subscripts o and p refer to the olefin and paraffin, respectively.

Division of one equation by the other yields

$$\frac{p_{p}}{p_{0}} \times \frac{p_{p}}{n_{p}} = \frac{Y_{p}}{X_{p}} \times \frac{X_{0}}{Y_{0}} = \frac{a_{0}b_{0}}{a_{p}b_{p}} = \text{constant}$$

where Y = mole fraction in gas phase, and X = mole fraction in adsorbate.

The left member of the above equation is analogous to the relative volatility for vaporliquid systems,⁷ hence the same terminology will be employed. The Langmuir equation states that at constant temperature the relative volatility of a binary mixture over an adsorbent is constant and independent of the adsorbate composition and the total pressure. For the system propane-propylene over the activated carbon used the relative volatility has been found to be substantially constant at barometric pressure at a value rather close to one. It is clear from Fig. 3 that such a low relative volatility means that the adsorbent does not differentiate greatly between these hydrocarbons.

(7) Walker, Lewis, McAdams and Gilliland, "Principles of Chemical Engineering," McGraw-Hill Book Co., New York, N. Y., 1937. March, 1950

In the case of silica gel as an adsorbent, it will be noted that the adsorption per gram on silica gel is less than that on activated carbon for each of the gases studied. The mixture behavior is also different. First, while there was little selection of one component over the other by the carbon, the silica gel differentiated rather strongly between the two gases with the result that propylene is, quite clearly, less volatile than propane. Second, the relative volatility is not independent of composition (as simple calculations will show), but varies markedly. Third, the affinity of silica gel for the hydrocarbon mixture not only is lower than the affinity of the activated carbon, but also it varies with compostion in an almost linear fashion.

It is to be noted that the adsorbent capacity has been based on the weight of adsorbent "as received." Since on an as received basis some three to five per cent. of the adsorbent weight is lost as a result of outgassing, the capacities reported are on the low side. This factor does not influence the mixture equilibrium results.

The data of Table IV indicate the high degree

of recoverability of the adsorbate. Within the limits of precision, recovery may be termed substantially complete.

Summary

In addition to the determination of the adsorption isotherms of propane and propylene on (a) activated carbon and (b) silica gel at $25.0 \pm 0.1^{\circ}$, the equilibrium behavior of binary mixtures of these two rather similar gases (physically) was also determined over each of the adsorbents at the same temperature. All adsorptions were entirely reversible.

There is very little difference in the relative volatility of these gases over activated carbon; there is substantial difference over silica gel. However, the adsorption capacity per unit weight of carbon is greater for these hydrocarbons than that of silica gel. In both these vapor-adsorbate equilibria propane is the more volatile component, whereas in the vapor-liquid equilibrium for this hydrocarbon system propane is the less volatile component.

CAMBRIDGE 39, MASS.

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Vapor-Adsorbate Equilibrium. II. Acetylene-Ethylene on Activated Carbon and on Silica Gel

BY W. K. LEWIS, E. R. GILLILAND, BERNARD CHERTOW AND W. MILLIKEN

Vapor-adsorbate equilibrium has been investigated for binary gaseous mixtures of acetylene and ethylene at 25.0° and barometric pressure. As in the previous work on propane-propylene mixtures¹ adsorption-desorption isotherms for each gas were determined on (a) activated carbon and (b) silica gel. Equilibrium data were collected with mixtures as in the earlier report, the equilibrium concentrations having been approached from both directions. In addition, desorption studies of mixtures permitted observations to be made on the reversibility of the adsorption.

Materials.—Commercial C. P. grade ethylene of 99.5 mole % minimum purity was employed. This gas was totally absorbed in 22% sulfuric acid saturated with mercuric sulfate² when its olefin content was determined. In addition, when subjected to a catalytic hydrogenation analysis³ the ethylene, after corrections were made for gas law deviations, was found to be 100% unsaturated.

The acetylene was drawn from commercial cylinders wherein it is kept in acetone solution.

(2) Francis and Lukasiewics, Ind. Eng. Chem., Anal. Ed., 17, 703 (1945).

According to the manufacturers, the acetylene contained in addition to acetone vapor the following as impurities

| | % | | % |
|-------|------|--|-------|
| O_2 | 0.03 | NH: | 0.005 |
| N_2 | .15 | H ₂ S | .005 |
| PH: | .026 | CO, CO ₂ , H ₂ , CH ₄ | .05 |

After a clean-up system (consisting of freshly de-aerated water for scrubbing out the acetone and sulfuric acid for drying) was installed, the acetylene purity was 99.2 mole % when determined in alkaline mercuric cyanide.⁴ The activated carbon, 28×60 mesh, was supplied by the Pittsburgh Coke and Chemical Company (Designation EY-51-C) and had a BET⁵ surface area of 805 sq. m. per g. The silica gel has already been reported on.¹

The apparatus and procedure were substantially those employed before¹ with but a modification in the determination of the acetylene isotherm. Because of about 0.8% unadsorbable impurity, it is obvious that any adsorption isotherm determined by successive additions of small known volumes of acetylene to a constant

(4) Wood, Fuel, 9, 289 (1930).

(5) Brunauer, Emmett and Teller, This Journal, 60, 309-319 (1938).

⁽¹⁾ W. K. Lewis, et al., THIS JOURNAL, 72, 1153 (1950).

⁽³⁾ R. F. Robey and C. E. Morrell, *ibid.*, 14, 880-883 (1942).